Development of a practical model to find out effectiveness of heat exchanger and its comparison with standard values

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Abstract—Exchange of heat from hot body to cold body or hot fluid to cold fluid will takes place by means of heat exchanging device. The device in which heat is transferred from hot fluid to cold fluid with maximum rate, minimum investment and less running cost is generally known as heat exchanger. The exchange of heat in heat exchanger may be in the form of sensible heat or latent heat or else it may be both latent and sensible heat. Usually the heat transfer in heat exchanger involves convection of fluids on each side and conduction through the wall that separates the two fluids. This paper focused on the development of a practical model with locally available materials to reduce the equipment cost and conducting experiment on it and studying its effectiveness for different flows like parallel flow, counter flow, crossed flow in the developed model, when hot and cold fluids flows through it. In heat exchanger when fluids are flowing hot fluid loses its temperature and cold fluid gain the temperature which is equivalent to fall of temperature by the hot fluid. This exchange heat relates with the length of heat exchanger. Readings recorded based on experiment and results are compared by different methods.

Keywords—LMTD, NTU, Effecteness, Parallel flow and counter flow

I. INTRODUCTION

Developing a practical Model to find out effectiveness of heat exchanger and its comparison involves three stages one is developing a practical model with locally available material, that involves purchasing suitable raw material and fabrication in to the shape and the second stage is conducting Experimentation on developed model on parallel flow and counter flow at different flow rates of hot and cold fluids and recording it readings and third stage involves calculation part for both parallel and counter flow to find out effectiveness by different methods like LMTD method, NTU method and comparison with heat transfer datebook values.

II. CLASSIFICATION OF HEAT EXCHANGERS

A. Based on the nature of heat exchange process
   • Direct contact type- here heat transfer takes place by direct mixing of hot and cold fluids

B. Based on the relative direction of fluid flow
   • Parallel flow heat exchanger- here both hot and cold fluid flow in the same direction
   • Counter flow heat exchanger – here hot and cold fluids flow in opposite direction
   • Cross flow heat exchangers-here the two fluids cross one another

C. Examples of heat exchangers
   • Condensers and boilers in steam plant
   • Intercoolers and pre heaters
   • Automobile radiators
   • Regenerators

III. EXPERIMENTAL SETUP

The apparatus consists of concentric tube of the heat exchangers. The hot fluid namely hot water is obtained from the Geyser (heater capacity 3 KW) and it flows through the inner tube. The cold fluid i.e. cold water can be admitted at any one of the ends enabling the heat exchanger to run as a parallel flow or as a counter flow exchanger. Measuring jar used for measure flow rate of cold and hot water. This can be adjusted by operating the different valves provided. Temperature of the fluid can be measured using thermocouples with digital display indicator. The outer tube is provided with insulation to minimize the heat loss to the surrounding.

Specifications:

- Specimen material: copper tube
- Size of the specimen: φ 19 mm X 1650 mm long
- Outer shell material: G.I Tube
- Size of outer shell: φ 38 mm
- Geyser capacity: 1 lit, 3 KW
Fig. 1. Experimental set up block diagram.

For parallel flow

\[ T_1 = \text{hot water inlet temperature in } ^\circ\text{C} \]
\[ T_2 = \text{hot water outlet temperature in } ^\circ\text{C} \]
\[ T_3 = \text{cold water inlet temperature in } ^\circ\text{C} \]
\[ T_4 = \text{cold water outlet temperature in } ^\circ\text{C} \]

For counter flow

\[ T_1 = \text{hot water inlet temperature in } ^\circ\text{C} \]
\[ T_2 = \text{hot water outlet temperature in } ^\circ\text{C} \]
\[ T_3 = \text{cold water outlet temperature in } ^\circ\text{C} \]
\[ T_4 = \text{cold water inlet temperature in } ^\circ\text{C} \]

With the above water flow arrangement the practical developed model is shown in below figure.

A. Experimental Procedure

- First switch on the unit panel
- Start the flow of cold water through the annulus and run the exchanger as parallel flow or counter flow
- Switch ON the Geyser provided on the panel and allow to flow through the inner tube by regulating valve.
- Adjust the flow rate of hot water and cold water by using rotameters and valves.
- Keep the flow rate same till steady state conditions are reached.
- Note down the temperatures of hot and cold water sides. Also note the flow rate.
- Repeat the experiment for different flow rates and for different temperatures. The same method is followed for counter flow also.

B. Experimental readings of Parallel flow arrangement

<table>
<thead>
<tr>
<th>Sno</th>
<th>Hot water flow rate ( m_w ), kg/s</th>
<th>Cold water flow rate ( m_c ), kg/s</th>
<th>Temp.of hot water(^\circ\text{C})</th>
<th>Temp.of cold water(^\circ\text{C})</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Inlet T1</td>
<td>Outlet T2</td>
<td>Inlet t1</td>
<td>Outlet t2</td>
</tr>
</tbody>
</table>

Fig. 2. Practically developed model of heat exchanger for parallel and counter flow.
1) Heat transfer for hot water.
a) \( Q_h = mh C_{ph}(T_1 - T_2) \) watts
b) \( mh \) = mass flow rate of hot water kg/sec
c) \( C_{ph} \) = specific heat of hot water = 4186.8 J kg-k
d) \( Q_h = 0.0227 \times 4186.8(47.2 - 42.6) = 437.185 \) watts.

2) Heat transfer for cold water.
a) \( Q_c = mc C_{pc}(t_1 - t_2) \) watts
b) \( mc \) = mass flow rate of cold water kg/sec
c) \( C_{pc} \) = specific heat of cold water = 4186.8 J kg-k
d) \( Q_c = 0.0416 \times 4186.8(29.4 - 25.8) = 627.015 \) watts.

3) \( Q = \frac{(Q_h + Q_c)}{2} \) watts.
\( Q = \frac{(437.18 + 627.0)}{2} = 532.09 \) watts.

4) \( LMTD = \frac{(\theta_1 - \theta_2)}{\ln(\theta_1/\theta_2)} \).
Where \( \theta_1 = T_1 - t_1 = 47.2 - 25.8 = 21.4 \) for parallel flow heat exchanger
\( \theta_2 = T_2 - t_2 = 42.6 - 29.4 = 13.2 \)
\( LMTD = \frac{(21.4 - 13.2)}{\ln(21.4/13.2)} = 16.971 \)

IV. OVERALL HEAT TRANSFER COEFFICIENT

Overall heat transfer coefficient is calculated based on outside surface area of inner tube which is as follows.

\[ U_o = \frac{Q}{A_o \times LMTD} \]

Where \( A_o = \pi \times d \times L \)
\( d_o = \text{outer diameter of the tube} = 0.019 \text{ m} \)
\( L = \text{length of the tube} = 1.65 \text{ m} \)
\( A_o = \pi \times 0.019 \times 1.65 \text{ m}^2 = 0.0985 \text{ m}^2 \)

\[ U_o = \frac{512.99}{0.0985 \times 16.977} = 318.191 \text{ W/m}^2 \text{-k} \]

V. TO FIND EFFECTIVENESS (\( \varepsilon \))

A. By using LMTD method

Find \( Ch \) = heat capacity rate of hot fluid
Heat carrying capacity of hot fluid \( Ch = mh \cdot C_{ph} \)
Heat carrying capacity \( Ch = 0.0227 \times 4186.8 = 95.040 \) (Min)

Find \( Cc \) = heat capacity rate of cold fluid
Heat carrying capacity of cold fluid \( Cc = mc \cdot C_{pc} \)
Heat carrying capacity of cold fluid \( Cc = 0.0416 \times 4186.8 = 174.170 \) (Max)

\( mh \) and \( mc \) are mass flow rate of hot and cold fluids
\( C_{ph} \) and \( C_{pc} \) are specific heat of hot and cold fluids J/kg-k

\[ \frac{C_{min}}{C_{max}} = \frac{95.040}{174.170} = 0.5456 \]

If \( Ch < Cc \) then effectiveness \( \varepsilon = \frac{T_1 - T_2}{T_1 - T_2} \) (hot fluid is min so this is applicable)
\[ \varepsilon = \frac{47.2 - 42.6}{47.2 - 25.8} = 0.214 \]

If Cc< Ch then effectiveness \( \varepsilon = \frac{T_2 - T_1}{T_2 - T_1} \)
This is applicable for both parallel and counter flow heat exchangers.

B. By using NTU method

1) \( NTU = \frac{(U_o \cdot A_o)}{C_{min}} \)

Note:
If \( Ch < Cc \) then \( Ch = C_{min} \) (hot fluid is minimum) and \( Cc = C_{max} \) (cold fluid is maximum)
If \( Cc < Ch \) then \( Cc = C_{min} \) (cold fluid is minimum) and \( Ch = C_{max} \) (hot fluid is maximum)

Where \( Ch = mh \cdot C_{ph} \) and \( Cc = mc \cdot C_{pc} \)

\[ NTU = \frac{218.191 \times 0.0985}{95.040} = 0.329 \]

2) Effectiveness of parallel flow heat exchanger.
\[ \varepsilon = \frac{1 - e^{-NTU(1+C)}}{1 + C} \]
\[ \varepsilon = \frac{1 - e^{-0.329(1+0.545)}}{1 + 0.545} \]
\[ \varepsilon = 0.29 \]

Note: effectiveness can also obtained by using chart from HMT data Book
Select NTU on X-axis and corresponding curve of \( C_{min} / C_{max} \) and read \( \varepsilon \) value on Y-axis.
Similarly for counter flow.
VI. EXPERIMENTAL READINGS FOR COUNTER FLOW ARRANGEMENTS

<table>
<thead>
<tr>
<th>Sno</th>
<th>Hot water flow rate ( m_h ), kg/s</th>
<th>Cold water flow rate ( m_c ), kg/s</th>
<th>Temp.of hot water°C</th>
<th>Temp.of cold water°C</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Inlet T1</td>
<td>Outlet T2</td>
<td>Inlet t1</td>
<td>Outlet t2</td>
</tr>
<tr>
<td>1</td>
<td>0.0227</td>
<td>0.0357</td>
<td>43.2</td>
<td>40.1</td>
</tr>
<tr>
<td></td>
<td>(250 ml/11s)</td>
<td>(250ml/7s)</td>
<td>26.6</td>
<td>30.2</td>
</tr>
</tbody>
</table>

A. Heat transfer for hot water

\[ Q_h = m_h \ C_{ph} (T_1 - T_2) \] watts

\( m_h = \) mass flow rate of hot water kg/sec

\( C_{ph} = \) specific heat of hot water = 4186.8 J kg\(^{-1}\)°C

\( Q_h = 0.0227 \times 4186.8 (43.2 - 40.1) = 294.625 \) watts

B. Heat transfer for cold water

\[ Q_c = m_c \ C_{pc} (t_1 - t_2) \] watts

\( m_c = \) mass flow rate of cold water kg/sec

\( C_{pc} = \) specific heat of cold water = 4186.8 J kg\(^{-1}\)°C

\( Q_c = 0.0357 \times 4186.8 (30.2 - 26.6) = 538.087 \) watts

C. \( Q = \frac{Q_h + Q_c}{2} \) watts

\( Q = (294.625 + 538.087) / 2 = 416.356 \) watts

D. \( \text{LMTD} = \frac{T_1 - T_2}{\ln \left( \frac{T_1 - T_2}{T_1 - T_2} \right)} \)

Where \( T_1 = T_1 - T_2 = 43.2 - 30.2 = 13 \) for counter flow heat exchanger

\( T_2 - t_1 = 42.6 - 26.6 = 13.5 \)

\( \text{LMTD} = \frac{13.5 - 13.2}{\ln(13.5)} = 13.24 \)

VII. OVERALL HEAT TRANSFER COEFFICIENT

Overall heat transfer coefficient is calculated based on outside surface area of inner tube

\( U_0 = \frac{Q}{A_0 X \text{LMTD}} \) W/m\(^2\)-k

Where \( A_0 = \pi \) do L

\( \text{do} = \) outer diameter of the tube = 0.019 m

\( L = \) length of the tube = 1.65 m

\( A_0 = \pi \times 0.019 \times 1.65 = 0.0985 \) m\(^2\)

\( U_0 = \frac{416.356}{0.0985 \times 13.24} = 319.257 \) W/m\(^2\)-k

VIII. TO FIND EFFECTIVENESS (\( \varepsilon \))

A. By using LMTD method

Find \( Ch = \) heat capacity rate of hot fluid

Heat carrying capacity of hot fluid \( Ch = m_h \ C_{ph} \)

\( \text{Heat carrying capacity } Ch = 0.0227 \times 4186.8 = 95.040 \) (Min)

Find \( Cc = \) heat capacity rate of cold fluid

Heating capacity of cold fluid \( Cc = m_c \ C_{pc} \)

Heating capacity of cold fluid \( Cc = 0.0357 \times 4186.8 = 149.468 \) (Max)

\( m_h \) and \( m_c \) are mass flow rate of hot and cold fluids

\( \text{Cph and Cpc are specific heat of hot and cold fluids J/kg-k} \)

\( Ch \) and \( Cc \) are heat carrying capacity of hot and cold fluids

\( Ch < Cc \), then effectiveness \( \varepsilon = \frac{T_1 - T_2}{T_1 - T_2} \) (hot fluid is minimum so this is applicable)

\( \varepsilon = \frac{43.2 - 40.1}{43.2 - 26.6} = 0.19 \)

\( Cc < Ch \), then effectiveness \( \varepsilon = \frac{T_1 - T_2}{T_1 - T_2} \)

This is applicable for both parallel and counter flow heat exchanger

B. By using NTU method

1) \( NTU = \frac{U_0 A_0}{C_{min}} \)

Note:

If \( Ch < Cc \) then \( Ch = C_{min} \) (hot fluid is minimum) and \( Cc = C_{max} \) (cold fluid is maximum)

If \( Cc < Ch \) then \( Cc = C_{min} \) (cold fluid is minimum) and \( Ch = C_{max} \) (hot fluid is maximum)

Where \( Ch = m_h \ C_{ph} \) and \( Cc = m_c \ C_{pc} \)

\( NTU = \frac{319.257 \times 0.0985}{95.040} = 0.33 \)

2) Effectiveness of parallel flow heat exchanger

\[ \varepsilon = \frac{1 - e^{-NTU(1-C)}}{1-e^{-NTU(1-C)}} \]

\[ \varepsilon = \frac{1 - e^{-0.33(1-0.635)}}{1-e^{-0.33(1-0.635)}} = 0.26 \]

Note: effectiveness can also obtained by using chart from HMT data Book
Select NTU on X-axis and corresponding curve of 
\( C=C_{\text{min}} / C_{\text{max}} \) and read \( \varepsilon \) value on Y-axis

Similarly for counter flow

IX. COMPARISON OF EFFECTIVENESS BY DIFFERENT METHODS

A. For parallel flow arrangement
   - By LMTD method: \( \varepsilon = 0.214 \)
   - By NTU method: \( \varepsilon = 0.29 \)
   - By using chart: \( \varepsilon = 0.28 \)

B. Comparison for counter flow arrangement
   - By LMTD method: \( \varepsilon = 0.19 \)
   - By NTU method: \( \varepsilon = 0.26 \)
   - By using chart: \( \varepsilon = 0.22 \)

CONCLUSION

The experimental data calculated and analyzed for parallel flow arrangement and counter flow arrangement by both methods of logarithmic mean temperature difference and NTU method and it was compared for both parallel and counter flow measurement and also the comparison is made for the both flows with the charts available in heat transfer data book and found the results obtained are almost giving the same effectiveness (matching) and hence the model developed is giving satisfactory results.

REFERENCES

[1] Engineering heat and mass transfer by Mahesh M.Rathore from university science press 113, golden house, daryaganj-New delhi-110002